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Parametric Study of an Organic Rankine Cycle Using Different Fluids

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Abstract

This work is an energy study of an organic Rankine cycle (ORC) for the recovery of thermal energy by comparing three organic fluids. This cycle is considered to be a promising cycle for the conversion of heat into mechanical energy suitable for low temperature heat sources; it uses more volatile organic fluids than water, which generally has high molecular weights, thus allowing operating pressures at temperatures lower than those of the traditional Rankine cycle. A thermodynamic model was developed using the Engineering Equation Solver (EES) software to determine its performance using different working fluids (toluene, R245fa and R123) under the same operating conditions, taking into account the effect of certain operating parameters and the selection of organic fluids on cycle performance. The results obtained show that the toluene organic fluid has the best thermal efficiency of the cycle compared to the other fluids; 14.38% for toluene, 13.68% for R123 and 13.19 for R245fa.

Keywords:

ORC Cycle; Energy Analysis; Organic Fluids; Performance.

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1- Introduction

A continuous increase in energy consumption has recently been observed due to the production process where certain environmental problems have been reported such as global warming and the depletion of fossil fuels. World energy consumption increased from 575 quadrillion British thermal units (Btu) in 2015 to 736 Btu quadrant in 2040, an increase of 28% (International Energy Outlook, United States, 2017); therefore, efficient systems are required by the integration of multiple power generation units, and as a result, a common primary energy supply can be used. It should be remembered that gas turbines in traditional thermal power plants use fossil fuels as a primary energy source in the production of electricity, where they use exhaust combustion gases to perform other thermal cycles such as than the Rankine vapor cycle, the organic Rankine cycle, absorption refrigeration cycles, desalination cycle and heating units [1, 2]. Studies and applications of Rankine Organic Cycle Systems (ORCs) have been steadily increasing in recent years due to their advantages in recovering heat from low temperature sources. Many researchers have studied the choice of working fluids; systems design methods, equipment and applications of ORC systems [3]. The Rankine organic cycle is one of the most commonly used technologies to generate electricity from low-content heat [4], which can be derived from geothermal energy [5-7], from biomass [8, 9], industrial waste [10] and solar energy [11, 12].

The organic fluids used by ORC systems are usually, Hydrofluorocarbon (HFC) refrigerants, ammonia (NH3), butane (C4H10), isopentane (C5H12), and toluene. Depending on the nature of the fluid, isentropic expansion from the dew curve may conserve, decrease, or increase the vapor titer. In fact, the slope of the dew curves in the Mollier diagram that explains this phenomenon specific to the nature of the fluid. A study was carried out by Feng et al. [4] on the experimental investigation of lubricating oil on a Rankine organic cycle (ORC) of 3 kW using R123. The effect of lubricant oil ratio using R123 on the system behavior under three different degree of superheating has been investigated [13]. Regarding the same topic area, by Yu et al. [14] conducted their study on the working fluids for

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Organic Rankine Cycles, their study show that the most energy-efficient working fluids are R125, R143a, R290 and R1270 for ORCs. Scaccabarozzi et al. [15] studied a Comparison of working fluids and cycle optimization for heat recovery ORCs from large internal combustion engines. In this work authors addresses the optimal working fluid selection for organic Rankine cycle recovering heat from heavy-duty internal combustion engines. Four cases are considered featuring two different engine exhaust temperatures (245 °C vs 354 °C) and two scenarios (maximum recovery of mechanical power vs. cogeneration of low-temperature heat). A new isothermal desalination system controlled by ORC has been studied experimentally, using the working fluid R245fa has been studied by Igobo et al. [16].

The purpose of this study is to estimate the mechanical power that can be provided by an organic ORC cycle, by studying the effect of the evaporation temperature and the choice of organic fluid that can adapt to this type of energy conversion system, and also to find the performance of the ORC cycle by comparing three different organic fluids (toluene, R245fa and R123).

2- Description of ORC Cycle

The heat transfer fluid at high temperature transfers the heat stored to the evaporator of the ORC cycle. This fluid can reach relatively high temperatures. The organic fluid pressurized by the pump is heated, then evaporated and superheated in the evaporator, by the heat energy from the heat source, transferred to the latter. The superheated steam obtained at the outlet of the evaporator drives the turbine, which is a rotational movement drives an alternator for the production of electricity. The steam at the outlet of the turbine is directed to the condenser where it is cooled by a flow of cooling water.



Figure 1. Scheme of Organic Rankine Cycle (ORC).

3- Thermodynamic Model

The ORC cycle is analyzed by applying the principle of conservation of mass and energy according to the first law of thermodynamics, for each of the four components of the organic Rankine cycle, taking the following hypotheses:

- Changes in kinetic energy and potential energy are negligible.
- The system is adiabatic (without thermal losses).
- The system operates at steady state.

3-1- Mass and Energy Balance of the ORC Cycle

The input and output mass flows are equal in steady state, we have:

$$\dot{m}_1 = \dot{m}_2 = \dot{m}_3 = \dot{m}_4 = \dot{m} \tag{1}$$

3-1-1- Pump

The circulation pump allows the movement of the organic fluid from the low-pressure condenser to the evaporator at high pressure; it is possible to determine the consumption of the pump. The energy balance of the pump is written as follows:

$$\dot{W}_P = \dot{m} \left(h_2 - h_1 \right) \tag{2}$$

The specific work consumed by the pump to compress the fluid is written:

$$\mathcal{W}_{P} = (h_{2} - h_{1}) = \nu(P_{2} - P_{1})$$
(3)

For an irreversible adiabatic compression, the mechanical efficiency of the pump is introduced as follows:

$$\eta_{P \, is} = \frac{W_{P \, r\acute{e}v}}{\dot{W}_{P \, irr\acute{e}v}} = \frac{W_{P \, is}}{\dot{W}_{P}} = \frac{(h_{2is} - h_{1})}{(h_{2} - h_{1})} \tag{4}$$

3-1-2- Evaporator

The working fluid enters the evaporator in the liquid state and heated therein at constant pressure P_2 to the evaporation temperature, then it evaporates at constant temperature and pressure. The energy balance of the evaporator is written as follows:

$$\dot{Q}_{Eavp} = \dot{m} \left(h_3 - h_2 \right) \tag{5}$$

3-1-3- Turbine

The expansion in the turbine is considered adiabatic and irreversible with a constant isentropic efficiency, which is defined as follows:

$$\eta_{T \, is} = \frac{\dot{W}_{T \, irr\acute{e}\nu}}{\dot{W}_{T \, r\acute{e}\nu}} = \frac{\dot{W}_{T}}{\dot{W}_{T \, is}} = \frac{(h_{3} - h_{4})}{(h_{3} - h_{4 \, is})} \tag{6}$$

The energy balance of the turbine is written as follows:

$$\dot{W}_T = \dot{m} (h_3 - h_4) = \dot{m} (h_3 - h_{4 \, is}) \eta_{T.m\acute{e}c} \tag{7}$$

The electric power of the turbine is given by:

$$\dot{W}_{T.ORC}^{elec} = \eta_{g\acute{e}n} * \dot{W}_{T.ORC} \tag{8}$$

3-1-4- Condenser

The working fluid enters the condenser in the vapor state, condenses at constant temperature and pressure, and exits in the liquid state where it yields a quantity of heat. The energy balance of the condenser is written as follows:

$$\dot{Q}_{Cond} = \dot{m}(h_4 - h_1) \tag{9}$$

Performances of the ORC system

The thermal efficiency of organic Rankine cycle is defined as:

$$\eta_{Th} = \frac{\dot{W}_{net.ORC}}{\dot{Q}_{Evp.ORC}} \tag{10}$$

$$\dot{W}_{net.ORC} = \dot{W}_T - \dot{W}_P \tag{11}$$

4- Results

In this part we compared the thermodynamic behavior of three types of organic fluids R245fa, R123 and toluene. The input parameters of the organic Rankine cycle operation are as follows: $T_{Evap} = 100$ °C; $T_{Cond} = 40$ °C; $\dot{m} = 1$ kg/s. The thermo-physical characteristics of the working fluids of the various points of the cycle are calculated using Engineering Equation Solver (EES) software [17]. Table 1 represents the thermodynamic characteristics of the various points of the ORC cycle for the three working fluids.

	T (°C)	P (bar)	h (kJ/kg)	S (kJ/kg.K)	x (-)			
	Working fluid: Toluene							
1	40	0.07907	-132.3	-0.3799	0			
2	40.02	0.7475	-132.3	-0.3799	1			
3	100	0.7475	347.1	0.9306	1			
4	45.37	0.07907	278.1	0.9306	1			
Working fluid: R123								
1	40	1.547	241.9	1.142	0			
2	40.25	7.868	242.3	1.142	1			
3	100	7.868	442.5	1.694	1			
4	50.08	1.547	414.6	1.694	1			
Working fluid: R245fa								
1	40	2.496	252.6	1.179	0			
2	40.4	12.69	253.4	1.179	1			
3	100	12.69	474.1	1.791	1			
4	50.44	2.496	444.2	1.791	1			

Table 1. Characteristic thermodynamic points of ORC cycle.

In order to jointly consider the fluid having the highest net mechanical power, and the best energy efficiency. This study allowed us to compare the behavior of different types of working fluid under similar conditions. The thermodynamic performances of the ORC cycle of the three fluids are shown in Table 2.

Table 2. Thermodynamic performance of the ORC cycle.

Donformonoog	Working fluids				
Performances	Toluene	R123	R245fa		
\dot{W}_{Pump} (kW)	0.1089	0.4445	0.7853		
$\dot{Q}_{Evp}(kW)$	479.4	200.1	220.8		
W _{Turbine} (kW)	69	27.82	29.91		
$\dot{Q}_{Cond}(kW)$	410.5	172,7	191.7		
W _{net.ORC} (kW)	68.92	27.38	29.12		
$\eta_{th.ORC}$ (%)	14.38	13.68	13.19		

The results show that the Toluene organic fluid appears to be a good compromise for these two criteria, it is the fluid that has the highest value of the net mechanical power $\dot{W}_{net.ORC} = 68.92 kW$ compared with the other fluid, it is also a fluid which presents the best energetic efficiency of the cycle which equals $\eta_{th.ORC-Toluene} = 14.38 \%$ compared to that of the organic fluid R123 $\eta_{th.ORC-R123} = 13.68 \%$ and that of the organic fluid $\eta_{th.ORC-R123} = 13.19 \%$.

In this part, we studied the influence of the evaporation temperature of the ORC cycle on the performances of the organic Rankine cycle, namely the net power delivered by the ORC cycle and the cycle efficiency using the three organic fluids. To do this by keeping the condensing temperature constant, that is to say by fixing the condensation temperature ($T_{cond} = 40$ °C), and by varying the evaporation temperature in the range of (80 - 150 °C).

Figure 2 shows the effect of the evaporation temperature on the net mechanical power provided by the ORC cycle for the three organic fluids used. The results show that the mechanical power supplied increases with the increase of the evaporation temperature for the three fluids. The mechanical power provided by the ORC cycle ranges from 43 kW to 118 kW for toluene. For the R123 and R245fa, the mechanical power ranges from 20 kW to 40 kW in the same temperature range.



Figure 2. Variation of mechanical power of Turbine with ORC evaporation temperature according to the studied working fluids

Figure 3 shows the effect of the evaporation temperature on the thermal power received by the evaporator to feed the organic Rankine cycle. The results show that the thermal power required for the supply of the ORC cycle is increased with the increase of the evaporation temperature, the working fluid Toluene uses a lot of energy during its vaporization at the evaporator. The thermal power received by the evaporator of the ORC cycle ranges from 450 kW to 550 kW for toluene; but the evaporation temperature does not affect the thermal power of the evaporator for R123 and R245fa.



Figure 3. Variation of thermal power of evaporator with ORC evaporation temperature according to the studied working fluids

Figure 4 shows the effect of the evaporation temperature on the thermal efficiency of the organic Rankine cycle. The results show that the thermal efficiency of the ORC cycle is increased with the increase of the evaporation temperature for the three fluids. The thermal efficiency of the ORC cycle ranges from 10.5 to 21.45 % for toluene. For the R123, the thermal efficiency ranges from 10.14 % to 19.69 %; in the same temperature range, the thermal efficiency ranges from 9.9 to 17.85 % for the R245fa. The Toluene fluid gives a very high performance relative to the other fluids.



Figure 4. Variation of Energy Efficiency with ORC evaporation temperature according to the studied working fluids

5- Conclusion

This work focused on the energy study of an Organic Rankine Cycle (ORC) for the production of electrical energy, based on the use of an organic fluid. From the results found, it was concluded that:

- The mechanical power supplied increases with the increase of the evaporation temperature for the three fluids.
- The thermal power required for the supply of the ORC cycle is increased with the increase of the evaporation temperature, the working fluid Toluene uses a lot of energy during its vaporization at the evaporator.
- The thermal efficiency of the ORC cycle is increased with the increase of the evaporation temperature for the three fluids.
- The Toluene fluid gives a better performance in terms of thermal efficiency relative to the other fluids.

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7- Conflict of Interest

The author declares that there is no conflict of interests regarding the publication of this manuscript. In addition, the ethical issues, including plagiarism, informed consent, misconduct, data fabrication and/or falsification, double publication and/or submission, and redundancies have been completely observed by the authors.

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